

SF-17, 17L, 18, 18L Type Safety Valve (Full Bore Type)

for (Pressure Vessels), (Steam Boiler), etc. (2.0MPa)



SF-17 Type



SF-18 Type

■ PRESSURE DIVISION

(MPa)

Code No.	Pressure division
1	1.0~1.3
2	Over 1.3~1.6
3	Over 1.6~2.0

■ SPECIFICATIONS

Model name	SF-17	SF-17L	SF-18	SF-18L
Code name	SF17-C □	SF17L-C □	SF18-C □	SF18L-C □
	※ Code No. of pressure division is required in □.			
Cap type	With lever		Without lever	
Applicable fluid	Air	Steam	Air, gases & liquids	Steam
Size	40~150(1½"~6")			
Fluid temperature	-5~235°C			
Set pressure range	1.0~2.0MPa			
End connection	Inlet: Flanged JIS 16K, 20KRF (Thickness is based on table of DIMENSIONS)* ¹ . Outlet: Flanged JIS 10KFF* ¹ , * ² .			
Materials	Body (Cast steel)* ³ , Disc & Seat ring (Stainless steel)			
	Disc & Seat ring: Stellite* ⁴ .			
Valve body pressure test	2 times of flange rated pressure. (Hydraulic)			

*1. Flange codes JIS B8210 10K(inlet) × JIS B2220 10K(outlet) and ASME(ANSI) Class 150 × 150 are also available upon your request.

*2. RF flange for outlet side is also available upon your request.

*3. For valve main body made of stainless steel, please contact our agent in your area.

*4. The valve for steam has split valve disc and only valve seat is stellite welded.

*5. For size 15~25mm, please see Page 82.

■ DIMENSIONS

(mm)

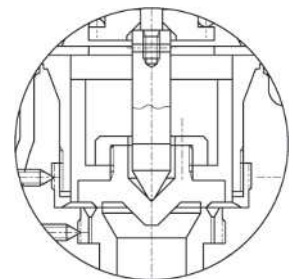
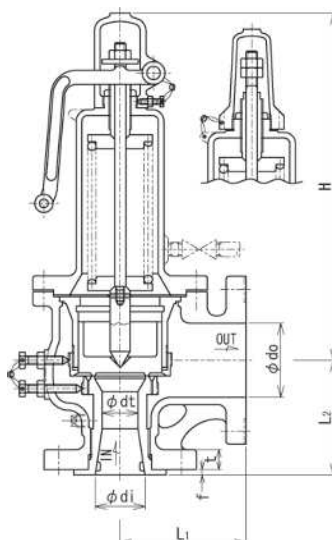
Size Inlet×Throat dia.×Outlet	Seat opening dia.	Throat dia.	Throat area	Lift	Face to Face		Height H		Thickness of flange		Mass(kg)	
							SF-17 SF-17L Type	SF-18 SF-18L Type			SF-17 SF-17L Type	SF-18 SF-18L Type
di×dt×do	D	dt	a(mm ²)	ℓ	L ₁	L ₂			t	f		
40(1½")×25 30×65(2½")	35	25 30	490.6 706.5	6.5 7.5	127	125	290	291	24	6	22	22
50(2")×34 38×80(3")	45	34 38	907.4 1133.5	8.5 9.5	136	135	374	375	26	6	30	29
65(2½")×43 49×100(4")	58	43 49	1451.4 1884.7	11.0 12.5	156	160	470	471	28	8	52	51
80(3")×55 61×125(5")	71	55 61	2374.6 2920.9	14.0 15.5	176	180	528	529	30	8	80	79
100(4")×69 76×150(6")	88	69 76	3737.3 4534.1	17.5 19.0	206	205	656	657	32	10	140	138
125(5")×86 95×200(8")	111	86 95	5805.8 7084.6	21.5 24.0	225	240	809	811	34	10	197	194
150(6")×105 115×200(8")	134	105 115	8654.6 10381.6	26.5 29.0	255	250	900	902	36	12	281	278

Note: The weight is that of JIS 20K inlet flange.

Flange code inlet JIS 16,20KRF
Outlet JIS 10K

■ CONSTRUCTION

● CONSTRUCTION OF SF-17L, 18L VALVE PART



Depending on nominal diameter, the structure of the valve may be different from what is shown in the drawing.

Extract from JIS B8210-2009 Spring Safety Valve for Steam and Gases

■ Allowed deviation of discharge-starting pressure

(1) For steam

There is no provision on the relief pressure of safety valve for steam.

(2) For gases

For valve for gases, the allowed deviation of start to discharge pressure is set pressure $\pm 5\%$ (minimum pressure: $\pm 0.025\text{MPa}$). In case of allowed deviation, which is not allowed to exceed set pressure, add the "+" side to "-" side.

Note: For valves for gases, the set pressure is generally the start to discharge pressure.

■ Allowed deviation of opening pressure (popping pressure)

(1) For steam

See Table 1 for the deviation of opening pressure. In case of allowed deviation, which is not allowed to exceed set pressure, add the "+" side to "-" side.

(2) For gases

For safety valves for gases, the allowed deviation of discharge-starting pressure is less than 1.1 times of start to discharge pressure. However, in the case of setting opening pressure, the deviation should be $\pm 3\%$ set pressure (minimum $\pm 0.015\text{MPa}$).

In case of allowed deviation, which is not allowed to exceed set pressure, add the "+" side to "-" side.

■ BLOWDOWN

(1) For steam

See Table 2 for the blowdown pressure of safety valves for steam. For valves for steam used with through flow boilers, re-heater, and piping, which opening pressure exceeds 0.3MPa , the blowdown pressure can be less than 10% of set pressure.

(2) For gases

See Table 3 for blowdown pressure of safety valves for gases.

Note: Unless otherwise specified in JIS B8210, Blowdown Standard of VENN shall apply.

■ Restriction of material use (pressure parts of safety valve) (Source: JIS B8210-2009)

(1) For steam

Material of pressure parts	Allowed range
Cast iron	Set pressure: Max. 1.6MPa . Fluid temperature: Max. 230°C
Ductile iron casting	Set pressure: Max. 2.4MPa . Fluid temperature: Max. 350°C

(2) For gases

Gas type	Toxic,flammable gases		Gases other than toxic,flammable gases	Toxic,flammable gases, other gases
	Allowed range			
Material of pressure parts				
Cast iron	Not allowed	Set pressure: Max.0.2 MPa		Not allowed
Ductile cast iron	Set pressure: Max.0.2 MPa	Set pressure: Max.1.6 MPa		Not allowed
Ductile iron casting	A: Application in system for highly toxic gases such as phosgene and hydrogen cyanide, etc is not allowed. B: For gases other than those mentioned in A, the set pressure should be Max. 2.4 MPa. C: Fluid temperature should be higher than -5°C and lower than 350°C.			

TABLE1. TOLERANCE OF OPENING PRESSURE OF SAFETY VALVES FOR STEAM

(MPa)

Set pressure	Tolerance
Below 0.5	± 0.015
0.5 or more and less than 2.3	$\pm (3\% \text{ of set pressure})$
2.3 or more and less than 7.0	± 0.07
7.0 or more	$\pm (1\% \text{ of set pressure})$

*1. For steam, generally the set pressure is assumed to be the opening pressure.

*2. The tolerance of the opening pressure of the safety valves for steam used other than in boilers can be $\pm 3\%$ of the set pressure (minimum value $\pm 0.015\text{MPa}$).

TABLE2. BLOWDOWN PRESSURE OF SAFETY VALVES FOR STEAM

(MPa)

Set pressure	Blowdown
0.4 or less	0.03
Over 0.4	7%(4%) or less of set pressure

*1. Generally, the blowdown pressure for steam shall be the difference between the opening pressure and the reseating pressure.

*2. The figures in () can be determined in accordance with the agreement between the parties concerned.

TABLE3. BLOWDOWN PRESSURE OF SAFETY VALVES FOR GASES

(MPa)

Set pressure	Blowdown	
	Metal seat type	Soft seat type
0.2 or less	0.03 or less	0.05 or less
Over 0.2	15% or less of set pressure	25% or less of set pressure

*1. Generally, the blowdown pressure for gases shall be the difference between the start to discharge pressure and the reseating pressure. However, when set by the opening pressure, it shall be the difference between the opening pressure and the reseating pressure.

*2. The definition of the soft seated and metal seated types shall be in accordance with JIS B0100.

Note. Unless otherwise specified in JIS B8210, Blowdown Standard of VENN shall apply.

DATA/Safety Valves, Relief Valves

Applicable Laws & Regulations and Formulas for Calculating Relieving Capacity

Coefficients assigned to equations may be those specified in applicable laws/regulations or in-house data(※).

※In-house data

1. PRESSURE VESSEL CONSTRUCTION CODE (from JIS B8210-2009)

(1) For Steam

$$Q_m = 5.25 C' K_{dr}' A P$$

Q_m: Relieving capacity (kg/h)A : Seat opening area (mm²)Lift type: $A = \pi D \ell$ Full bore type: $A = \frac{\pi d^2}{4}$

D: Seat opening diameter (mm)

ℓ: Lift (mm)

d: Throat diameter (mm)

P: Absolute relieving pressure (MPa·A)

(Select the larger one of set pressure × 1.1 + 0.101 or set pressure + 0.020 + 0.101.)

C': Coefficient determined according to the property of steam
(See Tab.1 in Page 87.)

For saturated steam, see the following table:

Absolute relieving pressure (MPa·A)	C': Coefficient determined according to the property of steam
Max. 0.5	1*
over 0.5~1.0	0.98*
over 1.0~2.0	0.97*
over 2.0	0.96*

For superheated steam, See Tab.1. in Page 87.

K_{dr}': Relieving coefficient

Lift type: 0.864*

Full bore type: 0.777

(2) For Gases

$$Q_m = C'' K_{dr} P_1 A K_b \sqrt{\frac{M}{ZT}}$$

Q_m: Relieving capacity (kg/h)A : Seat opening area (mm²)Lift type: $A = \pi D \ell$ Full bore type: $A = \frac{\pi d^2}{4}$

D: Seat opening diameter (mm)

ℓ: Lift (mm)

d: Throat diameter (mm)

Z: Compression coefficient: 1* (See Fig.1 in Page 90)

T: Absolute temperature (K) of gases at relieving pressure

P₁: Relieving pressure (MPa·A)

(Select the larger one of set pressure × 1.1 + 0.101 or set pressure + 0.020 + 0.101.)

P₂: Back pressure (MPa·A)

C'': Coefficient determined according to κ (See Tab.5 in Page 88)

κ : Adiabatic exponent (Isentropic, See Tab.4 in Page 88).

The value will be 1.001 if it is not specified, in which case C''=23.95

K_{dr}': Relieving coefficient

Lift type: 0.864*

Full bore type: 0.777

K_b: Back pressure compensation coefficient (Depending on P₂/P₁ and κ .
See Tab.6 in Page 89)

M: Molecular weight of gas (See Tab.4 in Page 88)

■ Calculating maximum flow-in gas using the following formula:

$$G = 0.0028 v \rho d^2$$

G: Flow in gas (kg/h)

v : Velocity of gas (m/sec)

(More than 20 for saturated steam, or more than 30 for super-heated steam, or more than 10 for common gas)

ρ : Density of gas (kg/m³)

d : Internal diameter of pipe (mm)

(3) For water/hot water (also applicable for hot water with temperature higher than 120°C)

(1) In case of searching from relieving capacity:

$$S = \frac{W}{87.7 / (P_1 + 0.1)^\kappa \gamma_1}$$

(2) In case of searching from thermal input of pressure vessel or thermal output of hot water boiler:

$$S = \frac{Q_\varepsilon}{87.7 C / (P_1 + 0.1)^\kappa \gamma_1}$$

(If (P₁+0.1)^κ > (P₁-P₂) in formula (1) and (2), replace (P₁-P₂) with (P₁+0.1)^κ)S : Seat opening area (mm²)

W: Relieving capacity of valve (kg/h)

P₁: Relieving pressure (MPa) (See Note)

Lift type: set pressure × 1.1

For SL-37~40, 43, 44 type, see Page 65.

Full bore type: select the larger one of set pressure × 1.15 or set pressure + 0.034

Relief valve (type E · ED): select the larger one of set pressure × 1.25
or set pressure + 0.034P₂: Outlet pressure (MPa)

κ : Coefficient correction (See Fig.2 in Page 90)

Δt: Difference between the saturated temperature of relieving pressure P₁ and the temperature of hot water at inlet. (°C)γ₁: Density of the hot water at inlet (kg/L) (See Tab.2 in Page 87)

Q : Thermal input of pressure vessel or thermal output of hot water boiler (kJ/h)

ε : Coefficient of volumetrical expansion for water(1/°C) (See Tab.3 in Page 87)

C: Specific heat of water at constant pressure (kJ/kg°C) (See Tab.3 in Page 87)

Note: In the case of full-bore valve and relief valve, make sure the relieving pressure (P₁) does not exceed "maximum working pressure of pressure vessel or hot water boiler X 1.1" or "maximum working pressure + 0.034".

Applicable Laws & Regulations and Formulas for Calculating Relieving Capacity

Coefficients assigned to equations may be those specified in applicable laws/regulations or in-house data (※).

※ In-house data

2. BOILER CONSTRUCTION CODE (from JIS B8210-2009)

(1) For Steam

$$Q_m = 5.25 C' K_{dr} A P$$

Q_m: Relieving capacity (kg/h)A : Seat opening area (mm²)Lift type: $A = \pi D \ell$ Full bore type: $A = \frac{\pi d^2}{4}$

D: Seat opening diameter (mm)

 ℓ : Lift (mm)

d: Throat diameter (mm)

P: Absolute relieving pressure (MPa·A)

(Select the larger one of set pressure $\times 1.03 + 0.101$ or set pressure $+ 0.015 + 0.101$)

C': Coefficient determined according to the property of steam (See Tab.1 in Page 87)

For saturated steam, see the following table:

Absolute relieving pressure (MPa·A)	C': Coefficient determined according to the property of steam
Max. 0.5	1※
over 0.5~1.0	0.98※
over 1.0~2.0	0.97※
over 2.0	0.96※

For superheated steam, see Tab.1 in Page 87.

K_{dr}: Relieving coefficient

Lift type: 0.864※

Full bore type: 0.777

(2) For hot water (applicable when temperature is less than 120°C. If temperature is higher than 120 °C, then use the formula described in (1))

(1) In case of searching from relieving capacity:

$$S = \frac{W}{87.7 / (P_1 + 0.1) \kappa \gamma_1}$$

(2) In case of searching from thermal input of pressure vessel thermal output of hot water boiler:

$$S = \frac{Q_e}{87.7 C / (P_1 + 0.1) \kappa \gamma_1}$$

In formula (i) and (ii), if $(P_1 + 0.1) \kappa > (P_1 - P_2)$, then $(P_1 + 0.1) \kappa$ should be replaced by $(P_1 - P_2)$.S: Seat opening area (mm²)

W: Required relieving capacity of valve (kg/h)

Note: In the case of full-bore valve and relief valve, make sure the relieving pressure (P₁) does not exceed "maximum working pressure of pressure vessel or hot water boiler $\times 1.1$ " or "maximum working pressure $+ 0.034$ ".P₁: Relieving pressure (MPa) (see Note)Lift type: set pressure $\times 1.1$

For SL-37~40, 43, 44 type see Page 65.

Full bore type: select the larger one of set pressure $\times 1.15$ or set pressure $+ 0.034$ Relief valve (type E · ED): select the larger one of set pressure $\times 1.25$ or set pressure $+ 0.034$ P₂: Outlet pressure (MPa) κ : Coefficient correction (See Fig.2 in Page 90) Δt : Difference between the saturated temperature of relieving pressure P₁ and the temperature of hot water at inlet. (°C) γ_1 : Density of the hot water at inlet (kg/L) (See Tab.2 in Page 87)

Q : Thermal input of pressure vessel or thermal output of hot water boiler (kJ/h)

 ε : Coefficient of volumetrical expansion for water (1/°C) (See Tab.3 in Page 87)

C: Specific heat of water at constant pressure (kJ/kg°C) (See Tab.3 in Page 87)

NOTE

It is necessary installing safety valve when water temperature exceeds 120°C. The formula is as the following:

$$Q_m = 5.25 C' K_{dr} A P$$

In this case, the required relieving capacity (kg/h) of safety valve can be calculated using the following formula:

$$W = \frac{Q}{h_1 - h_2}$$

W: Required relieving capacity of safety valve (kg/h)

Q: Thermal output of hot water boiler (kJ/h)

h₁: Enthalpy of saturated steam that is equivalent to the maximum working pressure of boiler (kJ/kg).h₂: Enthalpy of water supply (kJ/kg)

$$W = \frac{Q_e}{C}$$

 ε : Coefficient of volumetrical expansion of water (1/°C) (See Tab.3 in Page 87)

C: Specific heat of water at constant pressure (kJ/kg°C) (See Tab.3 in Page 87)

(3) For downtherm boiler

$$Q_m = C'' K_{dr} P_1 A K_b \sqrt{\frac{M}{ZT}}$$

Q_m: Relieving capacity (kg/h)A : Seat opening area (mm²)Lift type: $A = \pi D \ell$ Full bore type: $A = \frac{\pi d^2}{4}$

D: Seat opening diameter (mm)

 ℓ : Lift (mm)

d: Throat diameter (mm)

Z: Compression coefficient: 1※ (See Fig.1 in Page 90)

T: Absolute temperature (K) of gases at absolute relieving pressure

P₁: Absolute relieving pressure (MPa·A)(Select the larger one of set pressure $\times 1.1 + 0.101$ or set pressure $+ 0.020 + 0.101$)P₂: Absolute back pressure (MPa·A)C': Coefficient determined according to κ (See Tab.5, Page 88) κ : Adiabatic exponent (Isentropic, See Tab.4 in Page 88)

The value will be 1.001 if it is not specified, in which case C'=23.95

K_{dr}: Relieving coefficient

Lift type: 0.864※

Full bore type: 0.777

K_b: Back pressure compensation coefficient (Depending on P₂/P₁ and κ . See Tab.6 in Page 89)

M: Molecular weight of air (See Tab.4 in Page 88)

DATA/Safety Valves, Relief Valves

Applicable Laws & Regulations and Formulas for Calculating Relieving Capacity

Coefficients assigned to equations may be those specified in applicable laws/regulations or in-house data (※).

※In-house data

3. JIS B8210-2009: SPRING SAFETY VALVE FOR STEAM AND GAS

(1) For Steam

$$Q_m = 5.25 C' K_{d'} A P$$

Q_m: Relieving capacity (kg/h)A : Seat opening area (mm²)Lift type: $A = \pi D \ell$ Full bore type: $A = \frac{\pi d^2}{4}$

D: Seat opening diameter (mm)

ℓ: Lift (mm)

d: Throat diameter (mm)

P: Absolute relieving pressure (MPa·A)

Products for boiler: (Select the larger one of set pressure × 1.03 + 0.101 or set pressure + 0.015 + 0.101)

Products for pressure vessels: (Select the larger one of set pressure × 1.1 + 0.101 or set pressure + 0.020 + 0.101)

C': Coefficient determined according to the property of steam (See Tab.1 in Page 87.)

For saturated steam, see the following table:

Absolute flow rating pressure (MPa·A)	C': Coefficient depending on the nature of steam
Max. 0.5	1 [※]
Over 0.5~1.0	0.98 [※]
Over 1.0~2.0	0.97 [※]
Over 2.0	0.96 [※]

For superheated steam, See the table in Page 87.

K_{d'}: Relieving coefficientLift type: 0.864[※]

Full bore type: 0.777

(2) For Gases

$$Q_m = C'' K_{d'} P_1 A K_b \sqrt{\frac{M}{ZT}}$$

Q_m: Relieving capacity (kg/h)A : Seat opening area (mm²)Lift type: $A = \pi D \ell$ Full bore type: $A = \frac{\pi d^2}{4}$

D: Seat opening diameter (mm)

ℓ: Lift (mm)

d: Throat diameter (mm)

Z: Compression coefficient: 1[※] (See Fig.1 in Page 90)

T: Absolute temperature (K) of gases at relieving pressure

P₁: Absolute relieving pressure (MPa·A)

(Select the larger one of set pressure × 1.1 + 0.101 or set pressure + 0.020 + 0.101)

P₂: Absolute back pressure (MPa·A)

C'': Coefficient determined according to κ (See Tab.5 in Page 88)

κ : adiabatic exponent (See Tab.4, Page 88)

The value will be 1.001 if it is not specified, in which case C''=23.95

K_{d'}: Relieving coefficientLift type: 0.864[※]

Full bore type: 0.777

K_b: Back pressure compensation coefficient (Depending on P₂/P₁ and κ . See Tab.6 in Page 89)

M: Molecular weight of air (See Tab.4 in Page 88)

4. ELECTRICITY BUSINESS ACT (Technical Standard for Thermal Equipments for Power Generation) (Formula source: JIS B8210-1994)

■ Applicable for boilers and supporting equipments

(1) For Steam

$$Q_m = 5.246 C K_{d'} A (P + 0.1) \times 0.9$$

Q_m: Relieving capacity (kg/h)A : Seat opening area (mm²)Lift type: $A = \pi D \ell$ Full bore type: $A = \frac{\pi d^2}{4}$

D: Seat opening diameter (mm)

ℓ: Lift (mm)

d: Throat diameter (mm)

P: Relieving pressure (MPa)

Set pressure ≤ 0.1 MPa: Set pressure + 0.02

Set pressure > 0.1 MPa: Set pressure × 1.03

C: Coefficient determined according to the property of steam (See Tab.1 in Page 87)

Set pressure is < 0.5 MPa·A, at saturated pressure: 1

Set pressure is ≥ 0.5 MPa·A, at saturated pressure: 0.98

Superheated steam: Please contact our agent in your area.

K_{d'}: Rated discharge coefficientLift type: 0.96[※]

Full bore type: 0.864

(2) For Gases

$$Q_m = C' K_{d'} A P_1 \sqrt{\frac{M}{ZT}} \times 0.9$$

Q_m: Relieving capacity (kg/h)A : Seat opening area (mm²)Lift type: $A = \pi D \ell$ Full bore type: $A = \frac{\pi d^2}{4}$

D: Seat opening diameter (mm)

ℓ: lift (mm)

d: throat diameter (mm)

Z: Compression coefficient: 1[※] (See Fig.1 in Page 90)

T: Absolute temperature (K) of gases at absolute relieving pressure

C': Coefficient determined according to κ and P₂/P₁ (See Fig.3 in Page 90)κ : Adiabatic exponent (C_p/C_v) (See Tab.4 in Page 88)

The value is considered as 1 if it is not clear.

P₂: Absolute back pressure (MPa·A)K_{d'}: Relieving coefficientLift type: 0.96[※]

Full bore type: 0.864

P₁: Absolute relieving pressure (MPa·A)

(Absolute value of "set pressure × 1.1")

M: Molecular weight of gas (See Tab.4 in Page 88)

DATA/Safety Valves, Relief Valves

Applicable Laws & Regulations and Formulas for Calculating Relieving Capacity

Coefficients assigned to equations may be those specified in applicable laws/regulations or in-house data (※).

※In-house data

5. IN-HOUSE STANDARDS (for liquids other than water and hot water)

$$W=161 \times AK \sqrt{PG}$$

W: Relieving capacity (kg/h)

A: Seat opening area (mm²)

Lift type: A=πDℓ

Full bore type: A=0.785d²

D: Seat opening diameter (mm)

ℓ: Lift (mm)

d: Throat diameter (mm)

G: Specific gravity upon the inlet side temperature

P: Relieving pressure (MPa)

K: Flow coefficient

Lift type: 0.55 for upper guide type

0.45 for blade type

Full bore type: 0.60

[The value may be different depending on type and accumulation]

TABLE1. COEFFICIENT ACCORDING TO PROPERTY OF STEAM C'

(JIS B8210-2009)

Absolute pressure (MPa)	Temp. (°C)	Saturated temperature	200	220	240	260	280	300	320	340	360	380	400	420	440	460
0.5		1.004	0.994	0.971	0.950	0.931	0.912	0.895	0.879	0.863	0.848	0.834	0.821	0.808	0.796	0.784
1.0		0.986	0.980	0.982	0.960	0.938	0.919	0.900	0.883	0.867	0.852	0.837	0.824	0.810	0.798	0.786
1.5		0.976	0.975	0.969	0.969	0.946	0.925	0.906	0.888	0.871	0.855	0.843	0.826	0.813	0.800	0.788
2.0		0.971		0.966	0.963	0.955	0.932	0.912	0.893	0.875	0.859	0.844	0.829	0.815	0.802	0.790
2.5		0.968			0.960	0.965	0.940	0.918	0.898	0.880	0.863	0.847	0.832	0.818	0.805	0.792
3.0		0.966			0.961	0.956	0.948	0.925	0.904	0.884	0.867	0.850	0.835	0.821	0.807	0.794
4.0		0.964				0.957	0.953	0.939	0.915	0.895	0.875	0.857	0.841	0.826	0.811	0.798
5.0		0.965					0.955	0.952	0.929	0.905	0.884	0.865	0.847	0.831	0.816	0.802
6.0		0.968					0.962	0.953	0.943	0.917	0.893	0.873	0.854	0.837	0.821	0.807
7.0		0.971						0.959	0.954	0.930	0.904	0.881	0.861	0.843	0.826	0.811
8.0		0.975						0.968	0.956	0.944	0.915	0.890	0.869	0.849	0.832	0.816
9.0		0.980							0.963	0.960	0.927	0.900	0.877	0.856	0.837	0.820
10.0		0.987								0.972	0.962	0.941	0.911	0.885	0.863	0.843
12.0		1.000									0.977	0.973	0.935	0.904	0.878	0.856
14.0		1.019										0.982	0.964	0.926	0.896	0.870
16.0		1.039										1.005	1.001	0.952	0.916	0.886
18.0		1.068										1.044	1.007	0.977	0.933	0.903
20.0		1.100											1.036	1.011	0.958	0.917

* When pressure/temperature is an intermediate value, it is necessary to take the minimum value of absolute pressure/temperature division and do not apply the proportional method. When absolute pressure is below 0.5 MPa·A, then 0.5 MPa·A should be used as absolute pressure. For example, when relieving pressure (absolute pressure) is 1.6 MPa·A and temperature is 245°C, C' = 0.946.

TABLE2. HOT WATER SPECIFIC GRAVITY γ_t(kg/L)

(Source: Interpretation of Boiler Structure Standard)

Pressure MPa·A	0.1	0.2	0.4	0.6	0.8	1.0	1.2	1.4	1.6	1.8	2.0	2.2	2.5
40	0.992	0.992	0.992	0.993	0.993	0.993	0.993	0.993	0.993	0.993	0.993	0.993	0.993
50	0.998	0.988	0.988	0.988	0.988	0.988	0.989	0.989	0.989	0.989	0.989	0.989	0.989
60	0.983	0.983	0.983	0.983	0.983	0.984	0.984	0.984	0.984	0.984	0.984	0.984	0.984
70	0.978	0.978	0.978	0.978	0.978	0.978	0.978	0.978	0.978	0.978	0.979	0.979	0.979
80	0.972	0.972	0.972	0.972	0.972	0.972	0.972	0.972	0.972	0.972	0.973	0.973	0.973
90	0.965	0.965	0.965	0.965	0.965	0.966	0.966	0.966	0.966	0.966	0.966	0.966	0.966
100		0.958	0.958	0.958	0.958	0.959	0.959	0.959	0.959	0.959	0.959	0.959	0.959
110		0.951	0.951	0.951	0.951	0.951	0.951	0.951	0.951	0.951	0.952	0.952	0.952
120		0.943	0.943	0.943	0.943	0.943	0.943	0.943	0.944	0.944	0.944	0.944	0.944
130			0.935	0.935	0.935	0.935	0.935	0.935	0.935	0.935	0.935	0.936	0.936
140			0.926	0.926	0.926	0.926	0.926	0.926	0.927	0.927	0.927	0.927	0.927
150				0.917	0.917	0.917	0.917	0.917	0.917	0.918	0.918	0.918	0.918
160					0.907	0.908	0.908	0.908	0.908	0.908	0.908	0.908	0.908
170					0.897	0.897	0.898	0.898	0.898	0.898	0.898	0.898	0.898
180							0.887	0.887	0.887	0.887	0.888	0.888	0.888
190							0.876	0.876	0.876	0.877	0.877	0.877	0.877
200								0.865	0.865	0.865	0.865	0.865	0.865
210										0.853	0.853	0.853	0.853
220													0.841

Note: Intermediate value should be calculated using the proportional method.

* Water density should be "1" when temperature is lower than 40°C.

TABLE3. SPECIFIC HEAT AND EXPANSION COEFFICIENT OF HOT WATER

(Source: Interpretation of Boiler Structure Standard)

Temp. °C	Specific heat of water at constant pressure C _p kJ/kg°C	Expansion coefficient ε 1/°C
Below 40°C	4.150	0.00039
40	4.179	0.00039
50	4.181	0.00046
60	4.185	0.00053
70	4.190	0.00060
80	4.197	0.00066
90	4.205	0.00072
100	4.216	0.00079
110	4.229	0.00085
120	4.245	0.00090
130	4.263	0.00097
140	4.285	0.00103
150	4.310	0.00110
160	4.339	0.00118
170	4.371	0.00126
180	4.408	0.00134
190	4.449	0.00145
200	4.497	0.00155
210	4.551	0.00165
220	4.613	0.00179

Note: Intermediate value should be calculated using the proportional method.

DATA/Safety Valves, Relief Valves

Applicable Laws & Regulations and Formulas for Calculating Relieving Capacity

TABLE4. GAS PROPERTY

(JIS B8210-2009)

Gas names	Chemical symbol	Molecular weight M (kg/kmol)	Adiabatic (isentropic) index κ (1.013bar a, 15°C)	Critical pressure P_c (bar a.)	Critical temp. T_c (K)	Critical pressure ratio
Acetylene	C_2H_2	26.02	1.26	62.82	309.15	0.553
Air	—	28.96	1.40	37.69	132.45	0.528
Ammonia	NH_3	17.03	1.31	112.98	405.55	0.544
Argon	Ar	39.91	1.66	48.64	151.15	0.488
Normal butane	C_4H_{10}	58.08	1.11	36.48	426.15	0.583
Carbon dioxide	CO_2	44.00	1.30	73.97	304.25	0.546
Carbon monoxide	CO	28.00	1.40	35.46	134.15	0.528
Chlorine	Cl_2	70.91	1.35	77.11	417.15	0.537
Chlorofluoromethane	$CHClF_2$	86.47	1.18	49.14	370.15	0.568
Ethane	C_2H_6	30.05	1.22	49.45	305.25	0.561
Ethylene	C_2H_4	28.03	1.25	51.57	282.85	0.555
Hydrogen	H_2	2.015	1.41	12.97	33.25	0.527
Hydrogen chloride	HCl	36.46	1.41	82.68	324.55	0.527
Hydrogen sulfide	H_2S	34.08	1.32	90.08	373.55	0.542
Isobutane	$CH(CH_3)_2$	58.08	1.11	37.49	407.15	0.583
Methane	CH_4	16.03	1.31	46.41	190.65	0.544
Methyl chloride	CH_3Cl	50.48	1.28	66.47	416.25	0.549
Nitrogen	N_2	28.02	1.40	33.94	126.05	0.528
Nitrogen suboxide	N_2O	44.02	1.30	72.65	309.65	0.546
Oxygen	O_2	32.00	1.40	50.36	154.35	0.528
Propane	C_3H_8	44.06	1.13	43.57	368.75	0.579
Propylene	C_3H_6	42.05	1.15	46.60	365.45	0.574
Sulfur dioxide	SO_2	64.07	1.29	78.73	430.35	0.548

TABLE5. COEFFICIENT DEPENDING ON ADIABATIC (ISENTROPIC) EXPONENT (κ) (C'') (JIS B8210-2009)

κ	C''	κ	C''	κ	C''	κ	C''	κ	C''	κ	C''
0.41	16.65	0.71	20.96	1.01	24.04	1.31	26.41	1.61	28.34	1.91	29.96
0.42	16.82	0.72	21.08	1.02	24.12	1.32	26.49	1.62	28.40	1.92	30.01
0.43	17.00	0.73	21.20	1.03	24.21	1.33	26.56	1.63	28.46	1.93	30.06
0.44	17.17	0.74	21.31	1.04	24.30	1.34	26.63	1.64	28.52	1.94	30.10
0.45	17.33	0.75	21.43	1.05	24.39	1.35	26.69	1.65	28.58	1.95	30.15
0.46	17.50	0.76	21.54	1.06	24.47	1.36	26.76	1.66	28.63	1.96	30.20
0.47	17.66	0.77	21.65	1.07	24.56	1.37	26.83	1.67	28.69	1.97	30.25
0.48	17.82	0.78	21.76	1.08	24.64	1.38	26.90	1.68	28.74	1.98	30.30
0.49	17.98	0.79	21.87	1.09	24.72	1.39	26.97	1.69	28.80	1.99	30.34
0.50	18.13	0.80	21.98	1.10	24.81	1.40	27.03	1.70	28.86	2.00	30.39
0.51	18.29	0.81	22.09	1.11	24.89	1.41	27.10	1.71	28.91	2.01	30.44
0.52	18.44	0.82	22.19	1.12	24.97	1.42	27.17	1.72	28.97	2.02	30.49
0.53	18.58	0.83	22.30	1.13	25.05	1.43	27.23	1.73	29.02	2.03	30.53
0.54	18.73	0.84	22.40	1.14	25.13	1.44	27.30	1.74	29.08	2.04	30.58
0.55	18.88	0.85	22.51	1.15	25.21	1.45	27.36	1.75	29.13	2.05	30.63
0.56	19.02	0.86	22.61	1.16	25.29	1.46	27.43	1.76	29.18	2.06	30.67
0.57	19.16	0.87	22.71	1.17	25.37	1.47	27.49	1.77	29.24	2.07	30.72
0.58	19.30	0.88	22.81	1.18	25.45	1.48	27.55	1.78	29.29	2.08	30.76
0.59	19.44	0.89	22.91	1.19	25.53	1.49	27.62	1.79	29.34	2.09	30.81
0.60	19.57	0.90	23.01	1.20	25.60	1.50	27.68	1.80	29.40	2.10	30.85
0.61	19.71	0.91	23.11	1.21	25.68	1.51	27.74	1.81	29.45	2.11	30.90
0.62	19.84	0.92	23.20	1.22	25.76	1.52	27.80	1.82	29.50	2.12	30.94
0.63	19.97	0.93	23.30	1.23	25.83	1.53	27.86	1.83	29.55	2.13	30.99
0.64	20.10	0.94	23.39	1.24	25.91	1.54	27.93	1.84	29.60	2.14	31.03
0.65	20.23	0.95	23.49	1.25	25.98	1.55	27.99	1.85	29.65	2.15	31.07
0.66	20.35	0.96	23.58	1.26	26.05	1.56	28.05	1.86	29.71	2.16	31.12
0.67	20.48	0.97	23.67	1.27	26.13	1.57	28.11	1.87	29.76	2.17	31.16
0.68	20.60	0.98	23.76	1.28	26.20	1.58	28.17	1.88	29.81	2.18	31.21
0.69	20.72	0.99	23.86	1.29	26.27	1.59	28.23	1.89	29.86	2.19	31.25
0.70	20.84	1.001	23.95	1.30	26.34	1.60	28.29	1.90	29.91	2.20	31.29

Note: Intermediate value should be calculated using the interpolational method.

Calculation formula

$$C = 39.48 \sqrt{\kappa \left(\frac{2}{\kappa + 1} \right)^{\frac{\kappa + 1}{\kappa - 1}}}$$

DATA/Safety Valves, Relief Valves

3

SAFETY VALVES, RELIEF VALVES

Fig.1 Coefficient of compressibility Z (JIS B8210-2009)

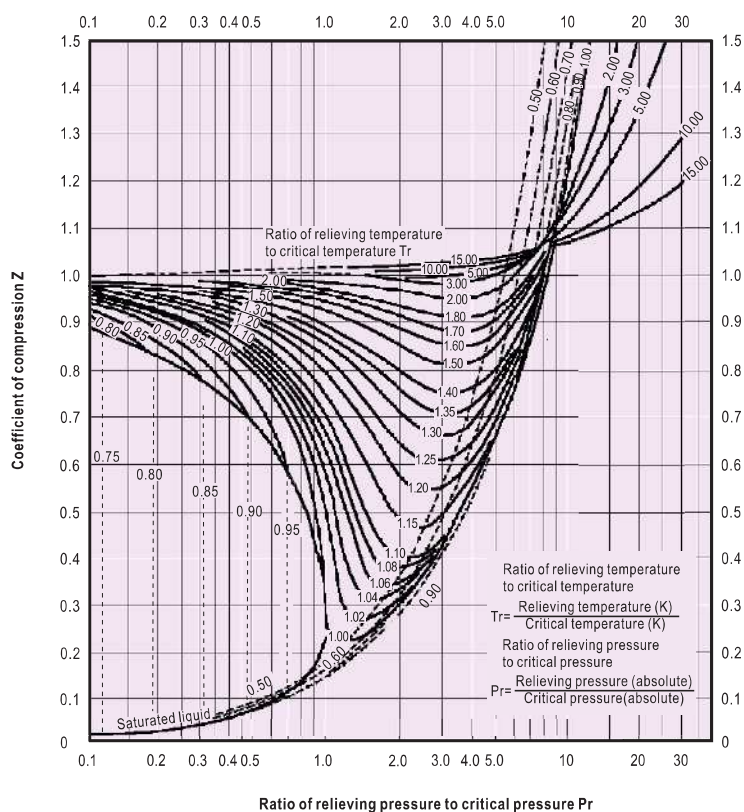


Fig.2 $\Delta t^\circ\text{C}$ correction coefficient κ

(Source: Interpretation of Boiler Structure Standard)

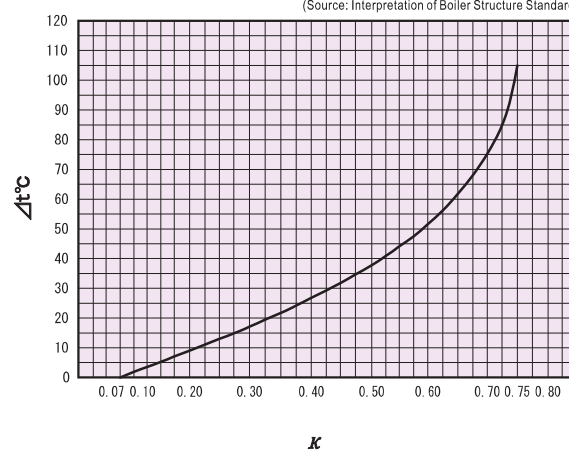
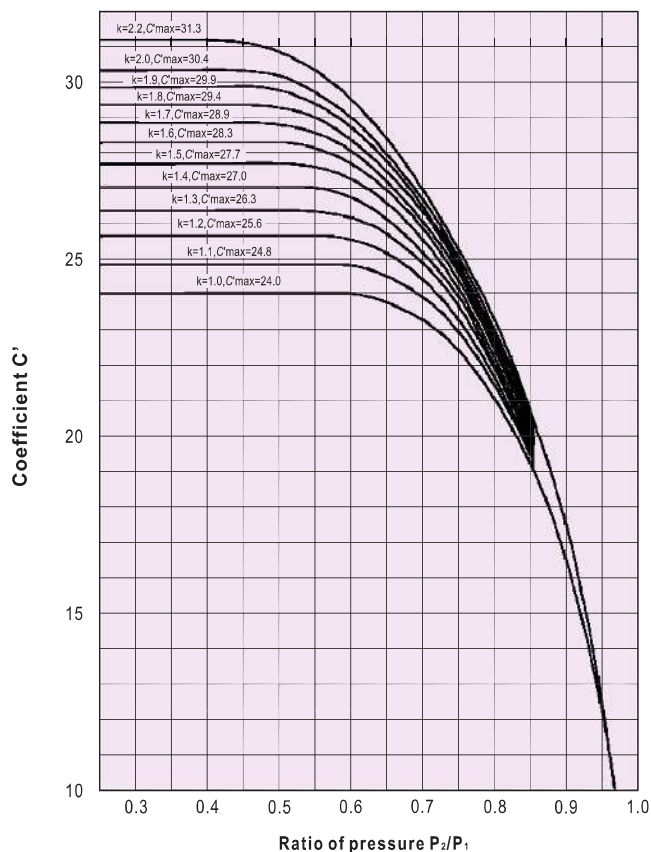


Fig.3 Coefficient (C') based on κ and P_2/P_1 (JIS B8210-2009)



Key Points for Installation of Safety Valves and Relief Valves

1. Installation

- ❶ Safety valve should be vertical to pipe. Before installation, remove scale and dust and clean the surfaces that contact with gasket.
- ❷ The diameter of the installation pipe should be larger than the diameter of valve. To reduce pressure loss to minimum degree, the stand pipe should be as short as possible.
- ❸ The stand pipe should be rigid and hard enough to bear the compression force, shearing force, bending stress or other counterforce caused by relieving of safety valve.
- ❹ Compared with the diameter of the outlet of safety valve, the diameter of the discharge pipe should be as large as possible. The discharge pipe should be as short as possible, without any bending, lead to outside of the door or other safe place, and be properly supported to avoid the occurrence of undesired stress (including thermal stress).

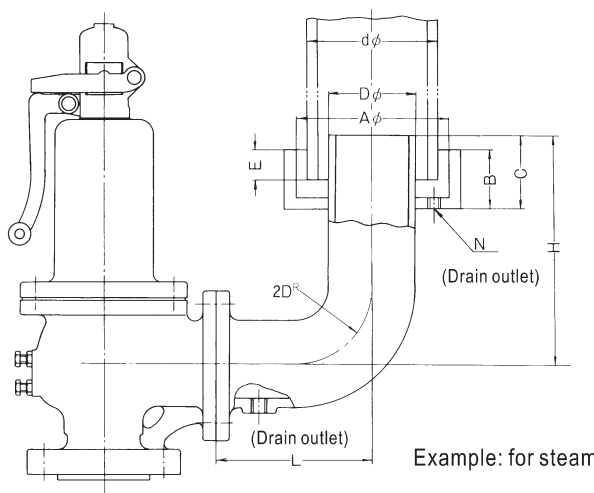
When deciding the place that the outlet of the discharge pipe faces, pay attention to the following issues.

- To avoid installation place where is influenced by explosive sound and blast.
- Avoid damage to electrical equipments, machines, tools etc. in the case the fluid is steam or water.
- Avoid corrosion, poisoning, anoxia etc. in the case the fluid is harmful gas.

- ❺ In the case of screwed type safety valve or relief valve, install union joint at the discharge pipe of the outlet side to allow easy dismounting (see Fig.1 in next page).
- ❻ At parts of the discharge pipe where drain or rain may accumulate, install the drain outlet, which is possible to discharge drain completely, and connect to dike.
- ❼ In the case of full bore type safety valve for liquids or harmful gases and have faucet for adjusting back pressure, install the valve on the outlet discharge pipe (see Fig.3 in next page).

- ❽ To avoid adverse impact on safety valve that is caused by thermal expansion of devices or discharge pipe, install proper expansion joint at the outlet of valve and install a discharge pipe at the end (see the figure below). To limit counterforce, the distance between the axes of the valve and the center of discharge pipe should be as short as possible, and the radius of the elbow pipe should be at least 2D (D: the internal diameter of the elbow). below figure also shows the standard dimensions of the discharge pipe of safety valve.

- ❾ Cares should be paid on installation of valves with lever (open type). It may effuse fluid from upper cap when such valves are operating (see Fig.5 in the next page).



REFERENCE DIMENSION FOR EXHAUST PIPE

(mm)

Outlet size	D	d	(A)	B	C	E	L	H	N
40(1½")	40	65	130	60	80	30	130	220	Rc¾"
50(2")	50	80	150	60	90	40	150	230	Rc½"
65(2½")	65	100	200	60	100	40	180	270	Rc½"
80(3")	80	125	200	70	120	50	200	310	Rc½"
100(4")	100	150	250	70	140	60	250	370	Rc¾"
125(5")	125	200	300	80	160	70	300	430	Rc1"
150(6")	150	200	300	80	180	70	350	500	Rc1"
200(8")	200	250	380	100	220	80	450	610	Rc1"

2. Maintenance and operating instructions

- ❶ At the installation of safety valves avoid the place where there is possibility to obstruct their functions by vibration or corrosion and do not give impact from outside.
- ❷ After installation, make sure the pressure of the device has reached at least 75% discharge pressure of the valve before using the test lever to start the valve.
- ❸ Normal working pressure of the equipment shall not exceed 90% of the blowdown pressure of the valve and 80 to 85% when pulsation is expected.

- ❹ If possible, remove safety valve before making water pressure test. To make water pressure test without removing safety valve, pay attention to the following below (see Fig.4 in the next page).
 - Ⓐ To prevent valve from being damaged due to improper load, when the pressure of the device reaches 80~90% of discharge pressure, install test gag* and press lightly on the end of valve shaft. The test gag must be rotated using hand. If you rotate it using

spanner or other tools, there may have excessively large pressing force, the seat may be damaged, the shaft may be bent, and the valve may not function normally.

- Ⓑ After water pressure test and the pressure reduces to 80~90% relieving pressure, remove test gag immediately.

※ The test gag is optional item.

Key Points for Installation of Safety Valves and Relief Valves

PIPING EXAMPLE

Fig.1 Example: Pressure tank installation

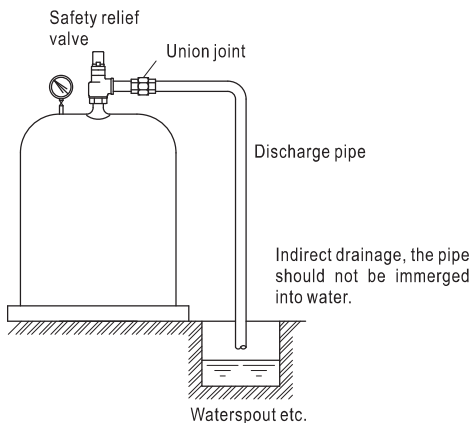


Fig.2 Example: Installation of the secondary side of pressure reducing valve

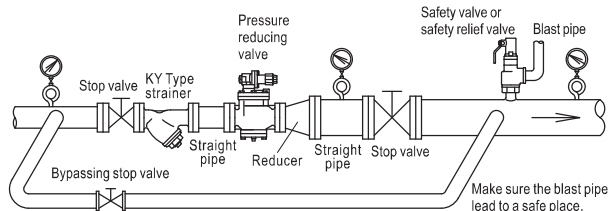


Fig.3 Example connection of back pressure adjusting cock

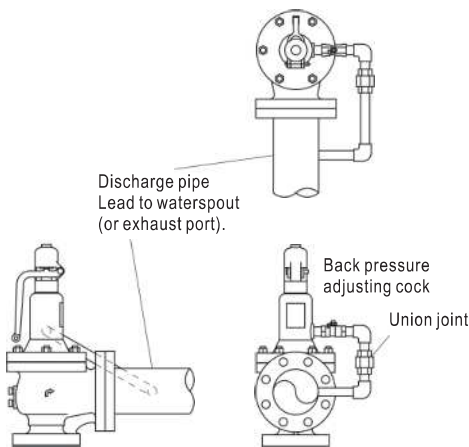


Fig.4 Installation of test gag

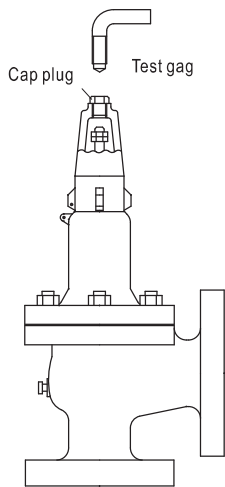


Fig.5 Lever structure

Lever structure of SL-37, 39, 39F,43 Type
For air, gas, or liquid

